

Elastic cells in uniform flow

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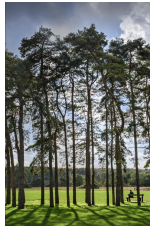
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Joint work with:

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Mark Blyth (UEA)



Applications

Unmanned aerial vehicles (UAVs)

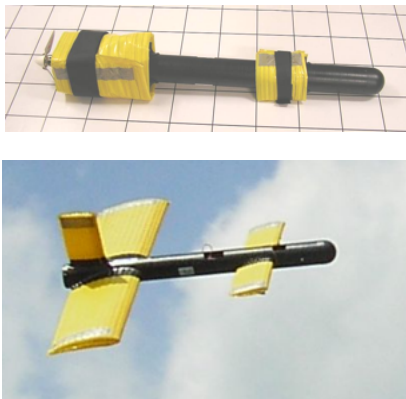
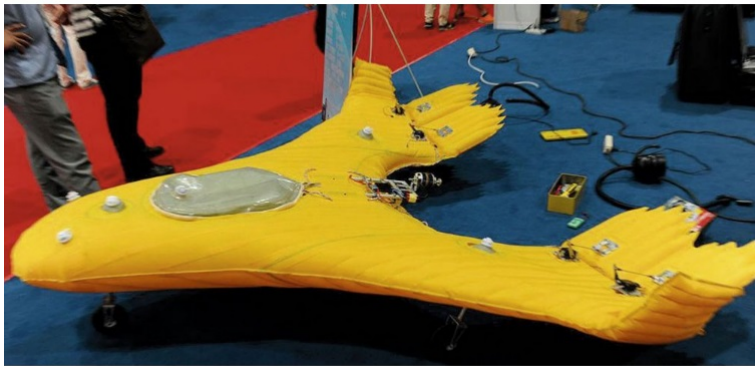


Figure: A UAV with inflatable elastic wings

- Advantages of UAV with inflatable wings: stowability, robustness,

...and inflatable drones



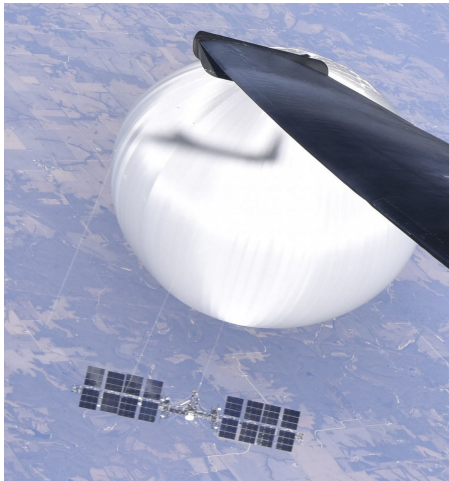
Advantages

Light, durable (likely to survive ground impact). Waterproof. Portability.

Review article

Li *et al.* (2018) A review of modelling and analysis of morphing wings

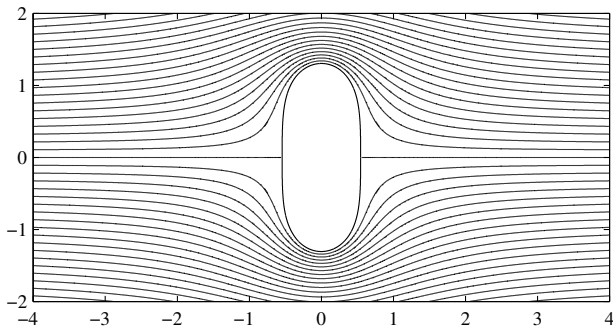
Chinese spy baloon



Wikipedia: 2023 Chinese balloon incident

Idealised Model

An elastic cell in a uniform stream



Inviscid, incompressible, irrotational flow

Related work

A two-dimensional bubble in a uniform stream

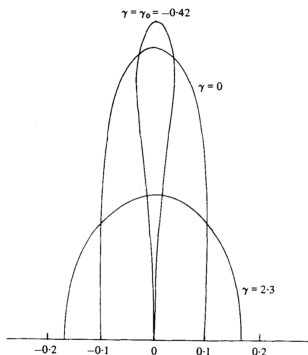


FIGURE 3. Same as figure 2 with $\beta = 90^\circ$ and $\gamma_0 = -0.42$. Each curve also represents half of a bubble in the absence of the wall.

Equilibrium states

- Vanden-Broeck & Keller (1980)
- Shankar (1992)
- Tanveer (1996)

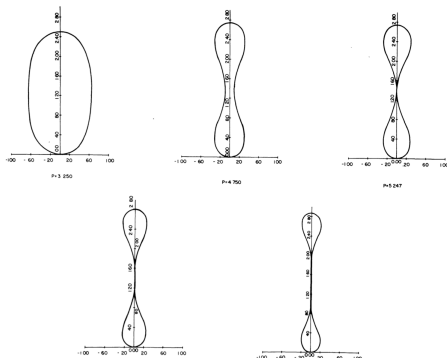
Stability

- Nie & Tanveer (1995)

[From: Vanden-Broeck & Keller (1980)]

Related work

Static, pressurised elastic cell

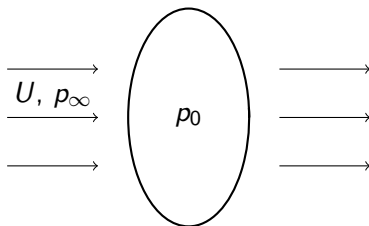


Buckled states

- Lévy (1884)
- Carrier (1947)
- Tadjbakhsh & Odeh (1967)
- Flaherty *et al.* (1972)

[From: Flaherty *et al.* (1972)]

Cell in a uniform stream



Complex potential:

$$\frac{dw}{dz} = u - iv, \quad z = x + iy \quad q = |w_z|$$

Far-field condition:

$$w \rightarrow Uz \quad \text{as} \quad z \rightarrow \infty$$

Bernoulli's equation:

$$\rho \operatorname{Re} \left(\frac{\partial w}{\partial t} \right) + \frac{1}{2} \rho q^2 + p = \frac{1}{2} \rho U^2 + p_\infty$$

Nondimensional governing equations

- Bernoulli's equation:

$$\operatorname{Re} \left(\frac{\partial w}{\partial t} \right) + \frac{1}{2}(q^2 - \alpha^2) - (\kappa_{ss} + \frac{1}{2}\kappa^3 - \sigma\kappa) - P = 0,$$

where $\alpha = \sqrt{\frac{L^3 \rho U^2}{8\pi^3 E_B}}$, $P = \frac{8\pi^3 L^3 (p_\infty - p_0)}{E_B}$.

- Inextensibility

$$\eta(s + 2\pi) = \eta(s),$$

- Kinematic condition

$$\boldsymbol{\eta}_t \cdot \hat{\mathbf{n}} = \mathbf{u} \cdot \hat{\mathbf{n}}.$$

- Far-field condition:

$$w \rightarrow \alpha z \quad \text{as} \quad |z| \rightarrow \infty$$

Steady state problem (no flow)

Flaherty *et al.* (1972)

($\alpha = 0$)

$$\kappa_{ss} + \frac{1}{2}\kappa^3 - \sigma\kappa + P = 0$$

Buckling pressures

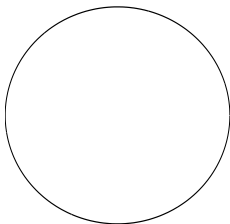
$$P = n^2 - 1 \quad n = 2, 3, 4, \dots$$

Contact pressures

$$P = 5.247, \quad P = 21.65, \quad P = 51.84$$

Buckling pressures

$$P = n^2 - 1 \text{ for } n = 2, 3, 4, \dots$$

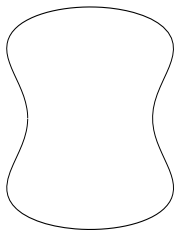


Pre-buckling pressure

$$P < 3$$

Buckling pressures

$$P = n^2 - 1 \text{ for } n = 2, 3, 4, \dots$$

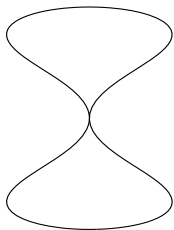


Mode 2 buckling

$$P > 3$$

Buckling pressures

$$P = n^2 - 1 \text{ for } n = 2, 3, 4, \dots$$

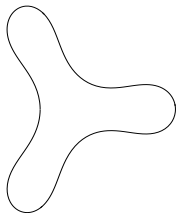


Mode 2 self-contact

$$P = 5.247$$

Buckling pressures

$$P = n^2 - 1 \text{ for } n = 2, 3, 4, \dots$$

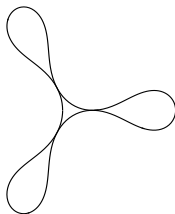


Mode 3 buckling

$$P > 8$$

Buckling pressures

$$P = n^2 - 1 \text{ for } n = 2, 3, 4, \dots$$

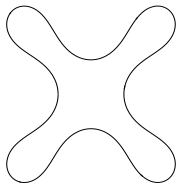


Mode 3 self-contact

$$P = 21.65$$

Buckling pressures

$$P = n^2 - 1 \text{ for } n = 2, 3, 4, \dots$$

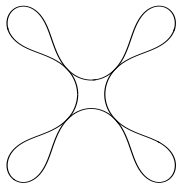


Mode 4 buckling

$$P > 15$$

Buckling pressures

$$P = n^2 - 1 \text{ for } n = 2, 3, 4, \dots$$

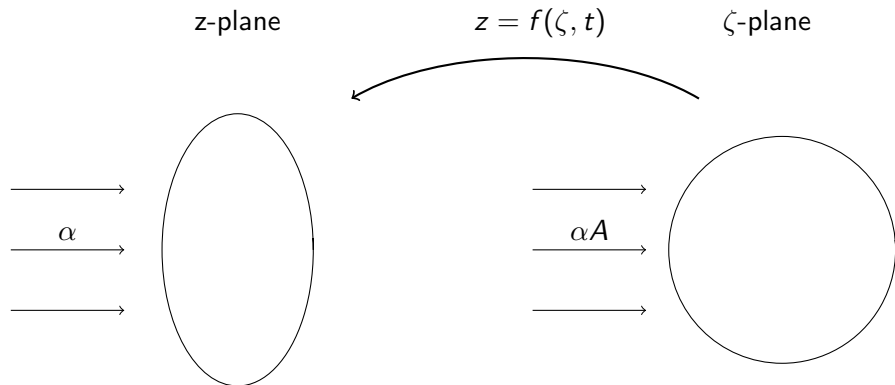


Mode 4 self-contact

$$P = 51.84$$

Conformal mapping

We seek a mapping from the flow around a circle (Shankar 1992)



Conformal mapping

We take the mapping functions to be

$$z = A(t)\zeta + a_0(t) + \sum_{n=1}^{\infty} a_n(t)\zeta^{-n},$$
$$w = \alpha A(t)\zeta + b_0(t) + \sum_{n=1}^{\infty} b_n(t)\zeta^{-n},$$

with the values on the cell wall given by the parametrisation $\zeta = e^{i\phi}$

$$\eta(\phi, t) = A(t)e^{i\phi} + a_0(t) + \sum_{n=1}^{\infty} a_n(t)e^{-in\phi},$$
$$\Omega(\phi, t) = \alpha A(t)e^{i\phi} + b_0(t) + \sum_{n=1}^{\infty} b_n(t)e^{-in\phi},$$

Governing equations

- Bernoulli's equation

$$\operatorname{Re} \left(\frac{\partial \Omega}{\partial t} - \frac{\Omega_\phi}{\eta_\phi} \frac{\partial \eta}{\partial t} \right) = -\frac{1}{2}(q^2 - \alpha^2) + \kappa_{ss} + \frac{1}{2}\kappa^3 - \sigma\kappa + P,$$

- Kinematic condition

$$\operatorname{Im}(\bar{\eta}_\phi \frac{\partial \eta}{\partial t}) = -\operatorname{Im}(\Omega_\phi)$$

- Inextensibility:

$$\int_0^{2\pi} |\eta_\phi| d\phi = 2\pi.$$

Steady solutions

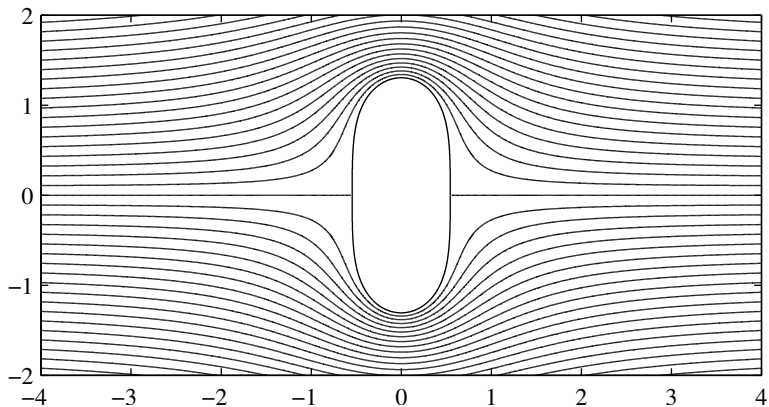


Figure: The vertically oriented steady solution at $\alpha = 1$, $P = 2$

Steady solutions

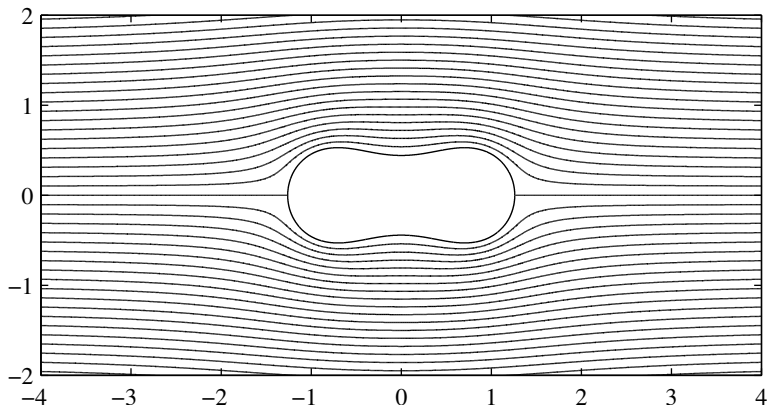


Figure: The horizontally oriented steady solution at $\alpha = 1$, $P = 4$

Steady solutions

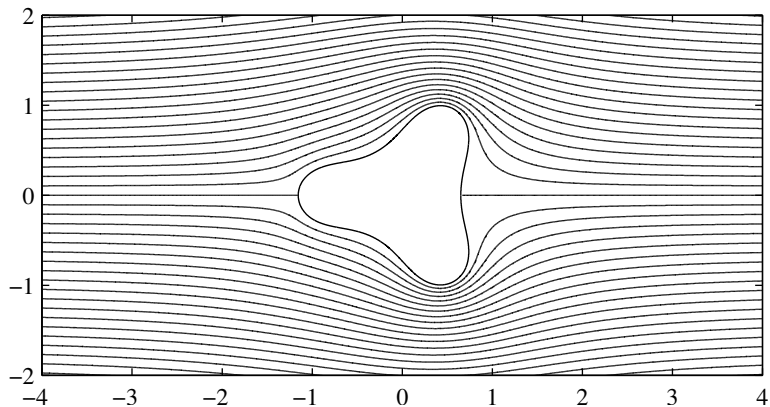


Figure: An asymmetric solution at $\alpha = 1$, $P = 9$

Steady solutions

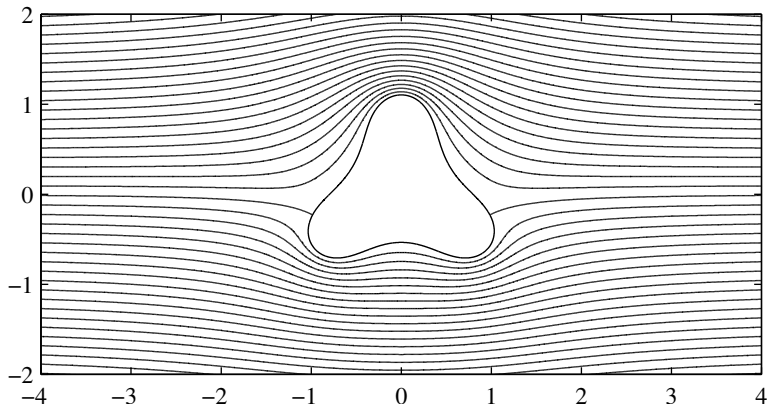


Figure: An asymmetric solution at $\alpha = 1$, $P = 9$

Steady solutions

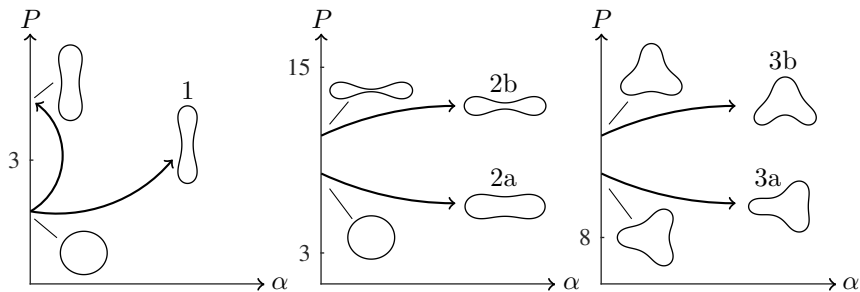


Figure: Sketch showing the classification of the steady solutions. At $\alpha = 0$, Flaherty *et al.* (1972). The arrows illustrate a continuous path taken to reach a particular cell type.

Linear stability of the steady solutions

To study the linear stability of the steady solutions, we introduce a small perturbation to both the cell boundary and the flow itself

$$\eta(\phi, t) = \eta^s(\phi) + \hat{\eta}(\phi, t), \quad \Omega(\phi, t) = \Omega^s(\phi) + \hat{\Omega}(\phi, t)$$

Taking a small perturbation $\hat{\mathbf{x}}(t) = \{\hat{a}_{1\dots n}, \hat{b}_{1\dots n}\}$, we obtain

$$A\hat{\mathbf{x}}_t = B\hat{\mathbf{x}},$$

where A and B depend on the steady terms a_n^s , b_n^s calculate above. Taking $\hat{\mathbf{x}}(t) = \hat{\mathbf{x}}_0 e^{\lambda t}$, we have

$$(A\lambda - B)\hat{\mathbf{x}}_0 = 0.$$

A steady solution is said to be spectrally stable if $\text{Re}(\lambda) \leq 0$ for all eigenvalues λ , and unstable otherwise.

Linear stability

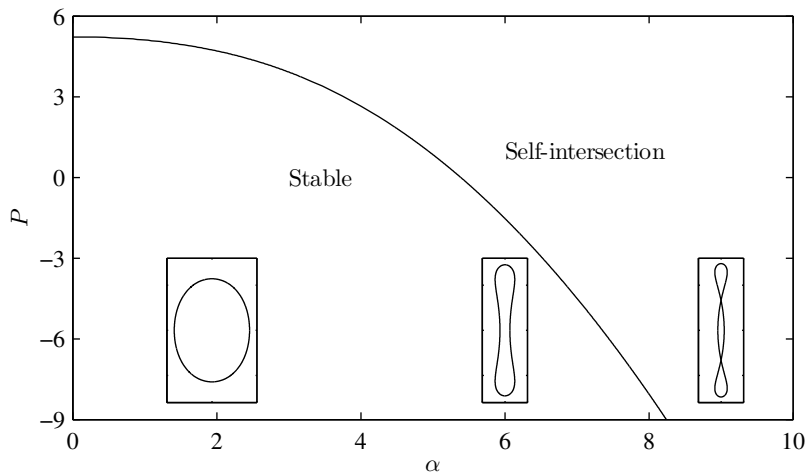


Figure: Properties of the vertically oriented cells.

Linear stability

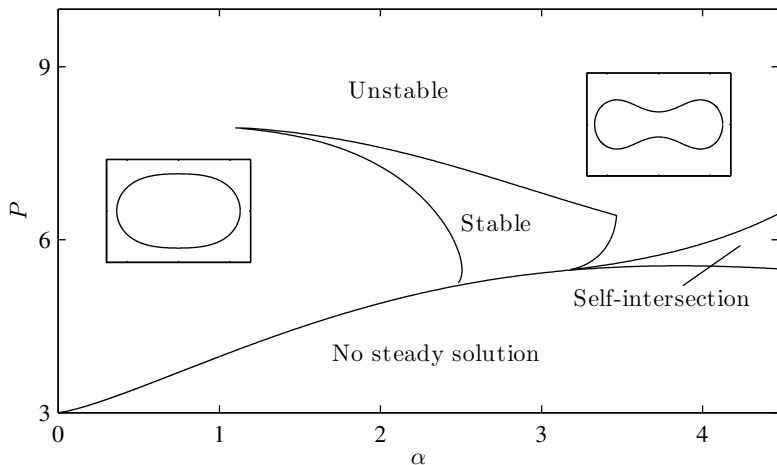


Figure: Properties of the horizontally oriented cells

Time-evolution of the fully nonlinear unsteady system

The governing equations are

$$\text{Im}(\bar{\eta}_\phi \frac{\partial \eta}{\partial t}) = -\text{Im}(\Omega_\phi)$$

$$\text{Re}\left(\frac{\partial \Omega}{\partial t}\right) = \text{Re}\left(\frac{\Omega_\phi}{\eta_\phi} \frac{\partial \eta}{\partial t}\right) - \frac{1}{2}(q^2 - \alpha^2) + \kappa_{ss} + \frac{1}{2}\kappa^3 - \sigma(t)\kappa + P,$$

$$\int_0^{2\pi} \kappa \text{Im}(\Omega_\phi) d\phi = 0.$$

where

$$\eta = A(t)e^{in\phi} + a_0(t) + \sum_{n=1}^{\infty} a_n(t)e^{-in\phi}$$

$$\Omega = \alpha A(t)e^{in\phi} + b_0(t) + \sum_{n=1}^{\infty} b_n(t)e^{-in\phi},$$

Numerical method

Using a Hilbert transform, we obtain an explicit system.

Kinematic condition:

$$\eta_t = i\eta_\phi \operatorname{Re} \left(\frac{i\Omega_\phi}{|\eta_\phi|^2} \right) + \eta_\phi \mathcal{H} \left(\operatorname{Re} \left(\frac{i\Omega_\phi}{|\eta_\phi|^2} \right) \right),$$

Bernoulli's equation:

$$\begin{aligned} \Omega_t = & \frac{\Omega_\phi}{\eta_\phi} \eta_t - \frac{1}{2}(q^2 - \alpha^2) + (\kappa_{ss} + \frac{1}{2}\kappa^3) + P \\ & + i\mathcal{H} \left(\frac{1}{2}u^2 - \kappa_{ss} - \frac{1}{2}\kappa^3 \right) + \sigma (i\mathcal{H}(\kappa) - \kappa), \end{aligned}$$

Inextensibility condition:

$$\int_0^{2\pi} \kappa_t \operatorname{Im}(\Omega_\phi) + \kappa \operatorname{Im}(\Omega_{\phi,t}) d\phi = 0.$$

Unstable eigenvalues for horizontally oriented cells

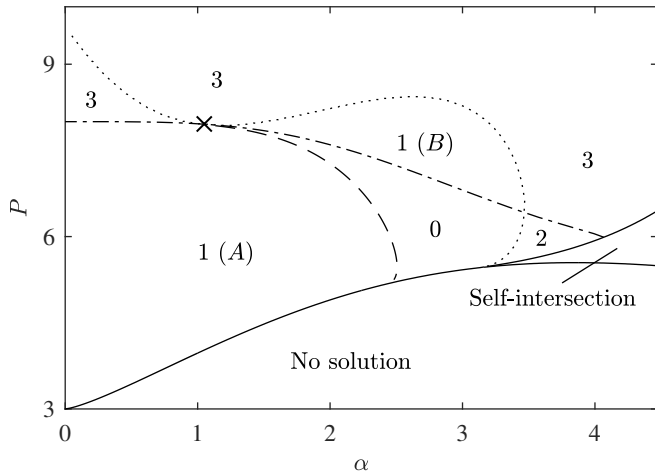
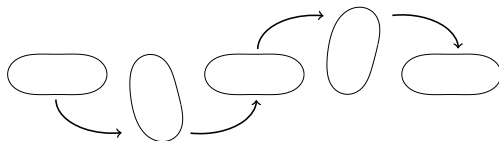


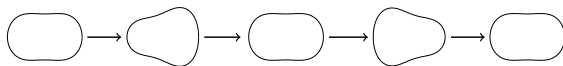
Figure: Properties of the horizontally oriented cells

Unsteady results: horizontally oriented cells

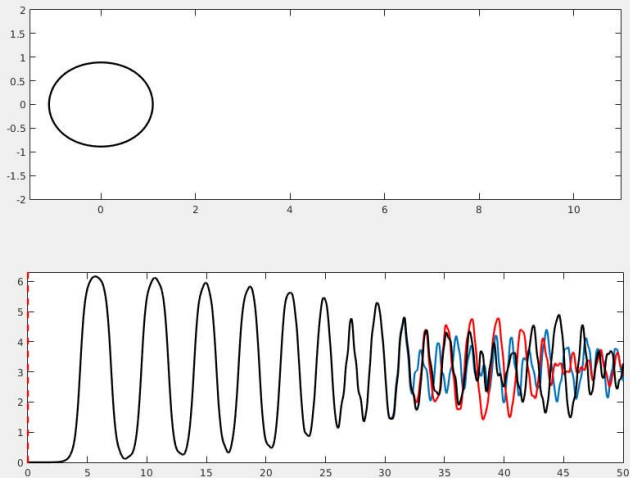
- (A) $\alpha = 2, P = 6$



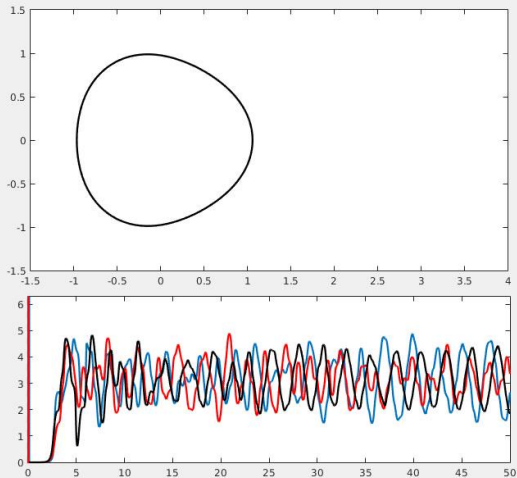
- (B) $\alpha = 2.5, P = 8$



Unsteady results: $\alpha = 1$, $P = 6$



Unsteady results: $\alpha = 0.5$, $P = 8.05$



Cells with corners

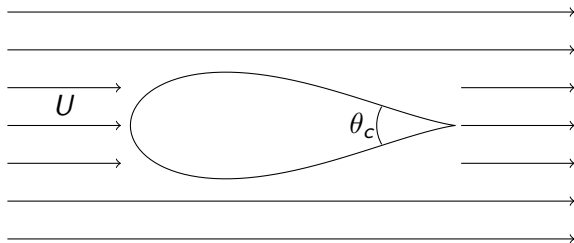


Figure: A sketch of the flow

$$q = 0 \quad \text{at} \quad s = 0, \quad \text{Kutta condition}$$

$$w - \alpha z - \frac{\beta}{2\pi i} \log(z) \rightarrow 0 \quad \text{as} \quad z \rightarrow \infty, \quad \text{far-field condition}$$

$$\frac{1}{2}(q^2 - \alpha^2) - (\kappa_{ss} + \frac{1}{2}\kappa^3 - \sigma\kappa) - P - \frac{\alpha\beta}{2\pi} (x_s + \kappa y) = 0.$$

with dimensionless parameters $\alpha = \sqrt{\frac{\ell^3 \rho U^2}{E_B}}$, $\beta = \Gamma \sqrt{\frac{\ell \rho}{E_B}}$.

Equilibria (no flow)

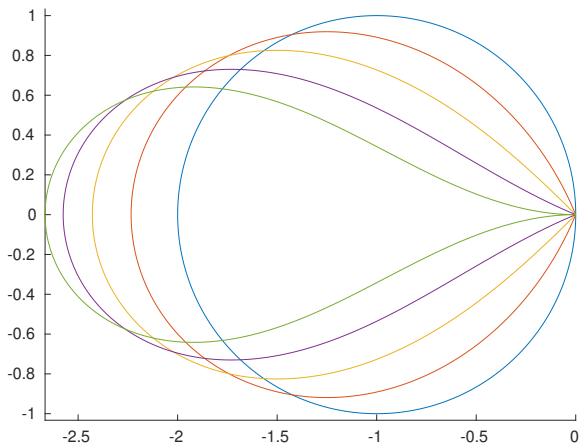
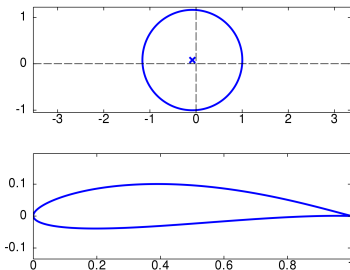


Figure: Cell subject to a uniform external pressure for various corner angles

Karman-Trefftz mapping for elastic aerofoil in uniform flow

ζ -plane (circle) $\rightarrow$ z -plane (aerofoil)

$$z = p \frac{(\zeta + 1)^p + (\zeta - 1)^p}{(\zeta + 1)^p - (\zeta - 1)^p}, \quad p = 2 - \frac{\theta_c}{\pi}$$



Cell with corner ($\beta \neq 0$) in the uniform flow

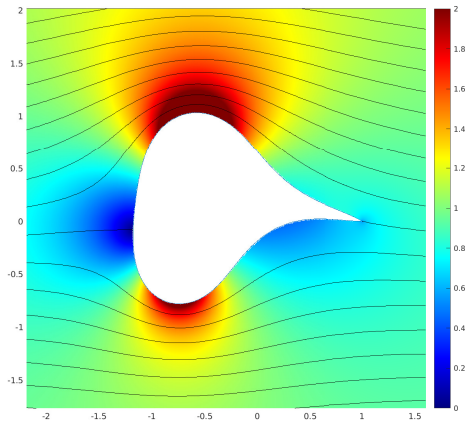
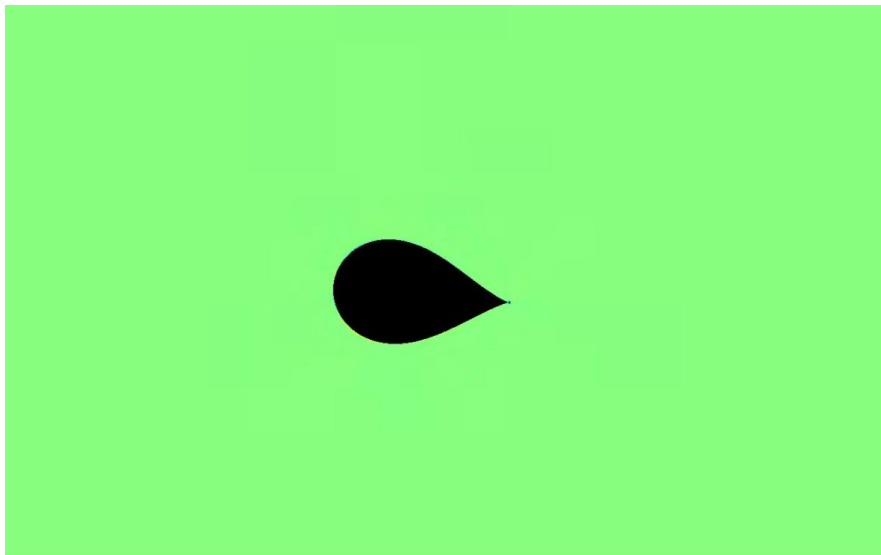


Figure: Potential flow for $\alpha = 2$, $P = 5$, $\beta = 3$, $\theta_c = \pi/6$

Viscous simulations



Gerris simulation for the viscous flow, with $Re = 10^4$, $\beta = \alpha = 1$, $P = 0$.

Other work

- Consider elastic cells with internal support

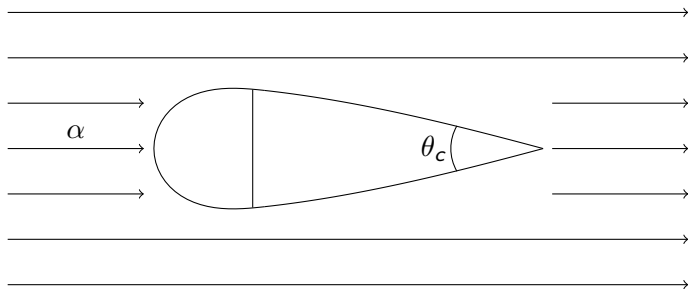


Figure: Sketch of the flow

References

1. M.G. Blyth, E.I. Părau, Deformation of an elastic cell in a uniform stream and in a circulatory flow, *IMA J. Applied Maths.* **78** (2013), 665-684
2. A. Yorkston, M. G. Blyth, E. I. Părau, The deformation and stability of an elastic cell in a uniform flow, *SIAM J. Appl. Math.* **80**(1), (2020), 71–94.
3. A. Yorkston, M. G. Blyth, E. I. Părau, A model of an inflatable elastic aerofoil, *J. Engng. Maths.* **131**, 11 (2021).
4. A. A. Yorkston, M. G. Blyth, E. I. Părau, The deformation of an elastic cell in a circulatory fluid motion, *Wave Motion* **13** (2022), 102995